# A NOTE ON MIXTURE DESIGNS DERIVED FROM FACTORIALS<sup>1</sup>

### By

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#### SUMMARY

The present paper provides an expression for the relation between the estimates of parameters of a linear model fitted through factorial design and those of the linear model fitted through the corresponding mixture design.

## 1. INTRODUCTION

Experiments for the study of response surfaces in which the response depends only on the relative proportions of the predictor variables  $x_i$ , in each combination, but not on their amounts, are termed as experiments with mixtures (Scheffe 1958, 1963). If  $x_i$  is the proportion of the *i*th component in an *n* component mixture, then

$$\sum_{i=1}^{n} x_i = 1, x_i \ge 0, i = 1, 2, ..., n. \qquad ...(1.1)$$

xi's are called mixture variables. Experimental designs for mixture experiments where in proportions for each component vary over the entire range 0 to 1 have been studied by Scheffe (1958, 1963) and Murty and Das (1968). Scheffe suggested the first and second degree polynomial functions for the response surfaces of mixture experiments, as

$$y_1 = \sum_{i=1}^{n} \beta_i x_i$$
 ...(1.2)

<sup>&</sup>lt;sup>1</sup>This work was first presented at the 33rd Annual Conference of the Indian Society of Agricultural Statistics held at Trichur in Dec., 1979. It was later included in [4].

and

$$M = \frac{1}{n(n-1)} \begin{bmatrix} n-1 & -1 & -1, & \dots & -1 \\ 0 & (n-2)f & -f, & \dots & -f \\ 0 & 0 & (n-3)g, -g, & -g, \\ & & & \ddots & \ddots & \\ 0 & 0 & \dots & k & -k \\ S & S & \dots & S & S \end{bmatrix} \dots (2.2)$$

in which the letters f, g, k, ... S are determined such that the sum of squares of each row is 1. Becker (1969) suggested an alternative transformation with

$$M = \begin{bmatrix} 1 - \frac{1}{n \pm \sqrt{n}}, \frac{-1}{n \pm \sqrt{n}} \end{bmatrix}_{n-1} \pm \frac{1}{\sqrt{n}} J_{n-1} \\ \frac{1}{\sqrt{n}} J'_{n-1} & \frac{1}{\sqrt{n}} \end{bmatrix} \dots (2.3)$$

where

 $[a, b]_r$ : is  $r \times r$  matrix with a as every diagonal element and every off diagonal element as b, and

 $J_{n-1}$ : (n-1)xl vector with every element unity.

Thompson and Myers (1968) suggested a matrix M in which the last row has different elements rather than identical elements as in (2.2) and (2.3).

## 3. THE LINEAR MODEL

Let  $w_{iu}$  denote the level of the  $i^{th}$  factor in the  $u^{th}$  combination (i=1, 2, ..., n-1; u=1, 2, ..., N) of W and  $y_u$  the corresponding response. Assuming that  $y_u$  is linearly related with  $(w_{1u}, w_{2u}, ..., w_{(n-1)u})$ , the linear model (1.4) in w's will be

$$E(Y) = (J: W) B$$
 ...(3.1)

where

Y':  $(y_1, y_2, \dots y_N)$ 

W: Nxn-1 factorial design matrix

 $B' : (b_0, b_1, ..., b_{n-1}).$ 

The least squares estimate of B is

$${}^{\wedge}_{B} \left[ (W'W)^{-1} W'y \right]. \qquad \dots (3.2)$$

If on the other hand, the response  $y_u$  is linearly related to  $(x_{1u}, x_{2u}, ..., x_{nu})$ , the model (1.2) will be

$$E(Y) = X\beta \qquad ...(3.3)$$

where

X :: Nxn mixure design matrix, and

 $\beta'$ :  $(\beta_1, \beta_2, ..., \beta_n)$  is a vector of unknown parameters.

The least squares estimate of  $\beta$  is

$$\hat{\beta} = (X'X)^{-1} X'Y. \qquad ...(3.4)$$

Since X and W are related by (2.1), we derive below the relation between  $\hat{\beta}$  and  $\hat{B}$ .

From (3.1) and (3.3), using (2.1),

$$(J W) \stackrel{\wedge}{B} = [(WO) M + J x'_0] \stackrel{\wedge}{\beta}.$$
 ...(3.5)

Writing 
$$M = \begin{bmatrix} M_1 \\ M_2 \end{bmatrix}$$
 ...(3.6)

we get

$$(JW) \stackrel{\wedge}{B} = (WM_1 + J \chi_0) \stackrel{\wedge}{\beta} \qquad ...(3.7)$$

$$= (J:W) \begin{pmatrix} x_0' \\ M_1 \end{pmatrix} \hat{\beta} \qquad \dots (3.7)$$

Assuming that (J:W) is of rank n

$$\hat{\beta} = \begin{pmatrix} x_0' \\ M_1 \end{pmatrix}^{-1} \hat{B} \qquad \dots (3.8)$$

The inverse in (3.8) can be evaluated using a result in Westlake (1968). Suppose the matrix  $P=(P_{ij})n$ , n differs from the matrix  $Q=(q_{ij})$  n, n in the  $k^{th}$  column. Then writing  $P^{-1}-(p^{ij})$ ,

$$q^{ij}=(q^{ij})$$
 and  $Z_1=\sum_{r=1}^n P^{ir} q_{rk}$ , we have  $q^{ij}=P^{ij}-Z_iq^{kj}$  for  $i\neq k$ ,  $q^{kj}=rac{P^{kj}}{Z_k}$  for  $i=k$ .

Now writing  $P' = (M_1' \ M_2'), \ Q = (M_1' \ X_0),$ 

and  $Z'=(Z_1, Z_2,..., Z_n)=(Mx_0')$ 

we get

$$\begin{pmatrix} x'_0 \\ M_1 \end{pmatrix}^{-1} = \begin{cases} \frac{m_{n_1}}{Z_n}, m_{11} - \frac{Z_1 m_{n_1}}{Z_n}, m_{21} - \frac{Z_2 m_{n_1}}{Z_n}, \dots, m_{n-1, 1} - \frac{Z_{n-1} m_{n_1}}{Z_n} \\ \frac{m_{n_2}}{Z_n}, m_{12} - \frac{Z_1 m_{n_2}}{Z_n}, m_{22} - \frac{Z_2 m_{n_2}}{Z_n}, \dots, m_{n-1, 2} - \frac{Z_{n-1} m_{n_2}}{Z_n} \\ \vdots & \vdots & \vdots & \vdots \\ \frac{m_{n_n}}{Z_n}, m_{1n} - \frac{Z_1 m_{n_n}}{Z_n}, m_{2n} + \frac{Z_2 m_{n_n}}{Z_n}, \dots, m_{n-1, n} - \frac{Z_{n-1} m_{n_n}}{Z_n} \end{cases}$$

$$[M'_{2}(M_{2}x_{0})^{-1}: M'_{1}-M'_{2}(M_{2}x_{0})^{-1}x'_{0}M'_{1}] \qquad ...(3.9)$$

If we assume  $M_2 = \frac{1}{\sqrt{n}} J_1$ , n as as in (2.2) and (2.3), then

$$M_2x_0 = \frac{1}{\sqrt{n}}$$
 and

$$\begin{bmatrix} x'_0 \\ M_1 \end{bmatrix}^{-1} = [J_n, _1: (I_n - J_{n_1} x'_0) M'_1] \qquad ...(3.10)$$

Therefore, from (3.9)

$$\hat{\beta} = J_{n, 1} : (I_n - J_{n, 1} x'_0) M'_1] \hat{B} \qquad ...(3.11)$$

In particular, if

$$x'_0 = \left(\frac{1}{n}, \frac{1}{n}, \dots, \frac{1}{n}\right) i.e.,$$

if the origin is shifted to the centroid of the simplex and M has the form given in (2.3) then

$$\hat{\beta} = (J: M_1) \hat{B}.$$
 ...(3.12)

From (3.1) the dispersion matrix of B is given by

$$D(\overrightarrow{B}) = \begin{bmatrix} J'J & J'W \\ W'J & W'W \end{bmatrix}^{-1} \sigma^2 \qquad ...(3.13)$$

When W represents a  $s^{n-1}$  factorial design with levels

$$0, \pm k_1, \pm K_2, \dots \pm \frac{k_{s-1}}{2}$$

it can be easily verified that

$$W'J=0 \text{ and}$$

$$W'W=\frac{2NK}{s}I_{n-1, n-1}$$
where
$$K=\sum_{i=1}^{\frac{S-1}{2}}k_1^2, N=s^{n-1}$$

$$\therefore D(\hat{B})=\begin{bmatrix} \frac{1}{N} & 0 \\ 0 & \frac{s}{2NK}I_{n-1, n-1} \end{bmatrix} \sigma^2 \qquad ...(3.15)$$

From (3.11)

From (3.11)
$$D(\hat{B}) = [J_{n, 1} : (I_{n} - J_{n, 1} x'_{0}) M'_{1}] \begin{bmatrix} \frac{1}{N} & 0 \\ 0 & \frac{s}{2NK} I_{n-1, n-1} \end{bmatrix}$$

$$\begin{bmatrix} J'_{1, n} & \\ M_{1} & I_{n} - Jx'_{0})'' \end{bmatrix} \sigma^{2} = \frac{JJ'}{N} + \frac{s}{2NK} (I_{n} - Jx'_{0}) (I'_{n} - Jx'_{0})' \sigma^{2}.$$
...(3.16)

#### ACKNOWLEDGEMENTS

The authors are thankful to the referee for the suggestions in improving the paper.

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